

# Tillinghast secondary tilts

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Sensoft analysis of TWFS images yields a prescription for adjustments of the secondary as “tilt M2 East by  $X$ ” and North by  $Y$ .” I calculate the numbers of turns of 2 of the 3 bolts that tilt M2 with respect to the optical axis to yield the Sensoft prescription.

Figure 1 is a low-quality reproduction of a photograph of a full-scale drawing of the back of the plate that holds M2. The 3 adjustment bolts are labeled A-C, and N marks the north direction. Figure 2 is a copy of a cut-out diagram (reduced from full-scale) along line AA in Figure 1, showing M2 and bolt A. Figure 3 is a diagram of the plate shown in Figure 1, with labels for the 3 bolts, the cardinal directions, and 2 known angles I use in the calculations. Various axes are also shown.

The Sensoft prescription gives the rotation angles  $\delta_E$  (tilt M2 East) and  $\delta_N$  (tilt M2 North). These are small angles in radians, so I treat them as vectors. When a bolt is turned, M2 rotates about the axis formed by the other 2 bolts. I’ll leave bolt A fixed, as we have 2 degrees of freedom. I picked A to remain fixed, because access to B and C is easier with the telescope tilted toward the mezzanine. Turning bolt B (C) then rotates M2 about axis AC (AB). These axes are shown in Figure 3 in green and red, respectively. In matching colors, axes parallel to AC and AB (A’C’ and A’’B’, respectively) are shown through the center of M2. These define angles  $\alpha$  (NA’) and  $\beta$  (NA’’) which relate small rotations about AB and AC to correspondingly small rotations about NS and EW:

$$\begin{aligned}\delta_E &= \delta_B \cos(\alpha) + \delta_C \cos(\beta) \\ \delta_N &= \delta_B \sin(\alpha) - \delta_C \sin(\beta)\end{aligned}\tag{1}$$

Figure 3 shows vectors representing  $\delta_B$  (green) and  $\delta_C$  (red). For small motions of the bolts, in the small-angle approximation  $\delta_B$  and  $\delta_C$  satisfy:

$$\delta_B = \frac{h_B}{R}, \quad \delta_C = \frac{h_C}{R}$$

where  $h_B$  and  $h_C$  are bolt displacements (positive away from M2) and  $R$  is the distance from each bolt to its corresponding axis of rotation (e.g., B to AC), which in turn is equal to the radius of the bolt circle multiplied by 1.5, from the geometry. The signs of  $\delta_B$  and  $\delta_C$  are such that positive  $h_B$  and  $h_C$  produce CCW rotations about AC and AB, respectively. These displacements satisfy:

$$h_B = \frac{T_B}{P_{mm}}, \quad h_C = \frac{T_C}{P_{mm}}$$

where  $T_B$  and  $T_C$  are the numbers of CW turns of the bolts and  $P_{mm}$  is the pitch of the bolts in turns per mm.

Solving eqn. 1 for  $\delta_B$  and  $\delta_C$  yields:

$$\begin{aligned} T_B &= RP_{mm} \frac{\delta_E \sin(\beta) + \delta_N \cos(\beta)}{\sin(\alpha + \beta)} \\ T_C &= RP_{mm} \frac{\delta_E \sin(\alpha) - \delta_N \cos(\alpha)}{\sin(\alpha + \beta)} \end{aligned} \quad (2)$$

The quantities required to calculate  $T_B$  and  $T_C$  are:

$$\begin{aligned} \alpha &= 7.55^\circ \\ \beta &= 52.45^\circ \\ R &= 1.5 \times 187. \text{ mm} \\ P_{mm} &= \frac{24 \text{ turns/inch}}{25.4 \text{ mm/inch}} \end{aligned}$$

The Sensoft prescription based on the best data from 23 March 2009 is:

$$\begin{aligned} \delta_N &= 80.2'' \\ \delta_E &= 188.2'' \end{aligned}$$

Using the equations above and scaling the prescription from arcsec to radians, I obtained:

$$\begin{aligned} T_B &= 0.294 \\ T_C &= -0.081 \end{aligned}$$

These are very small turns, so I conclude that we are reasonably close to a good collimation.

We will test TWFS further by turning bolts one at a time and acquiring images to verify that Sensoft yields the appropriate corrections.

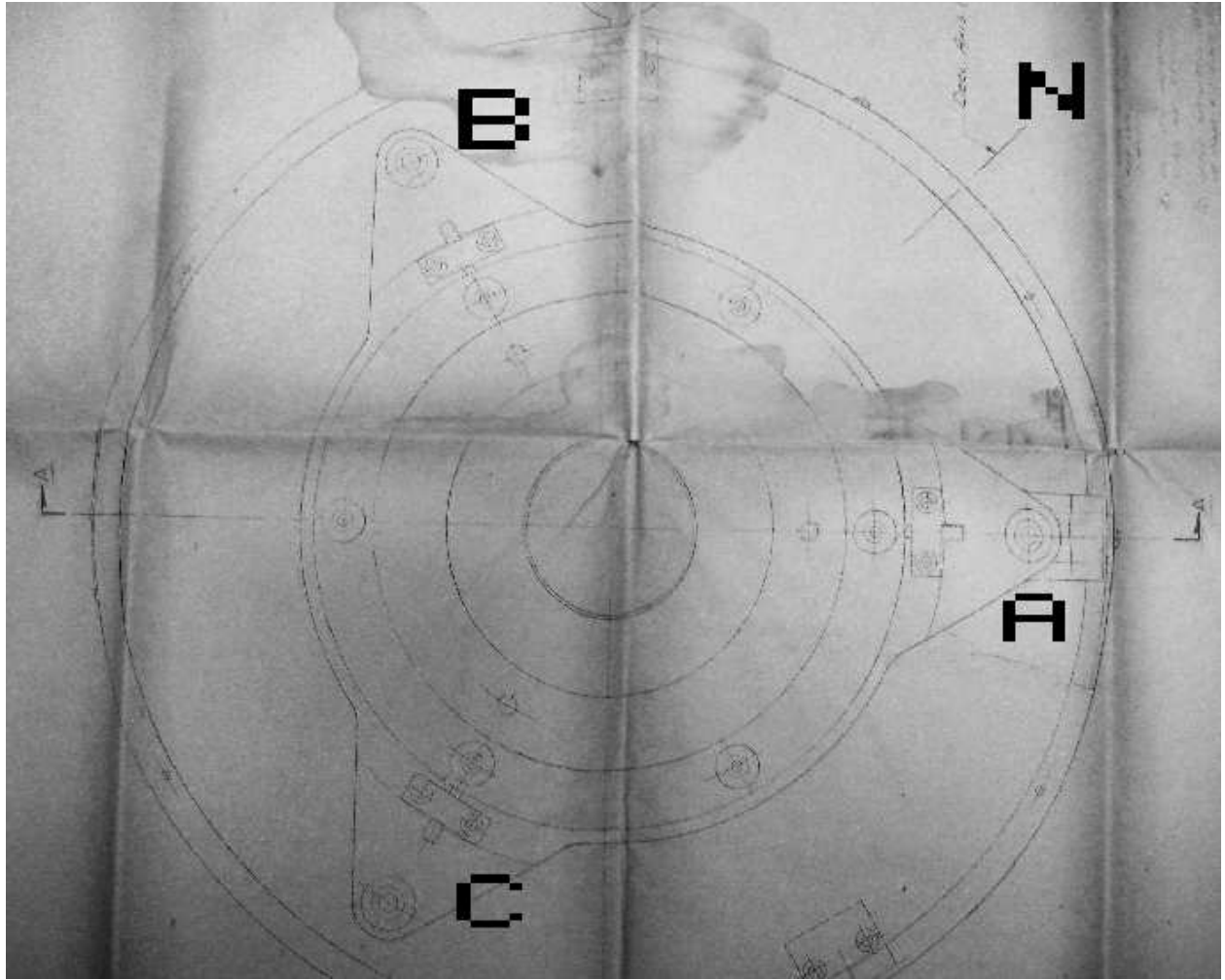


Fig. 1.—

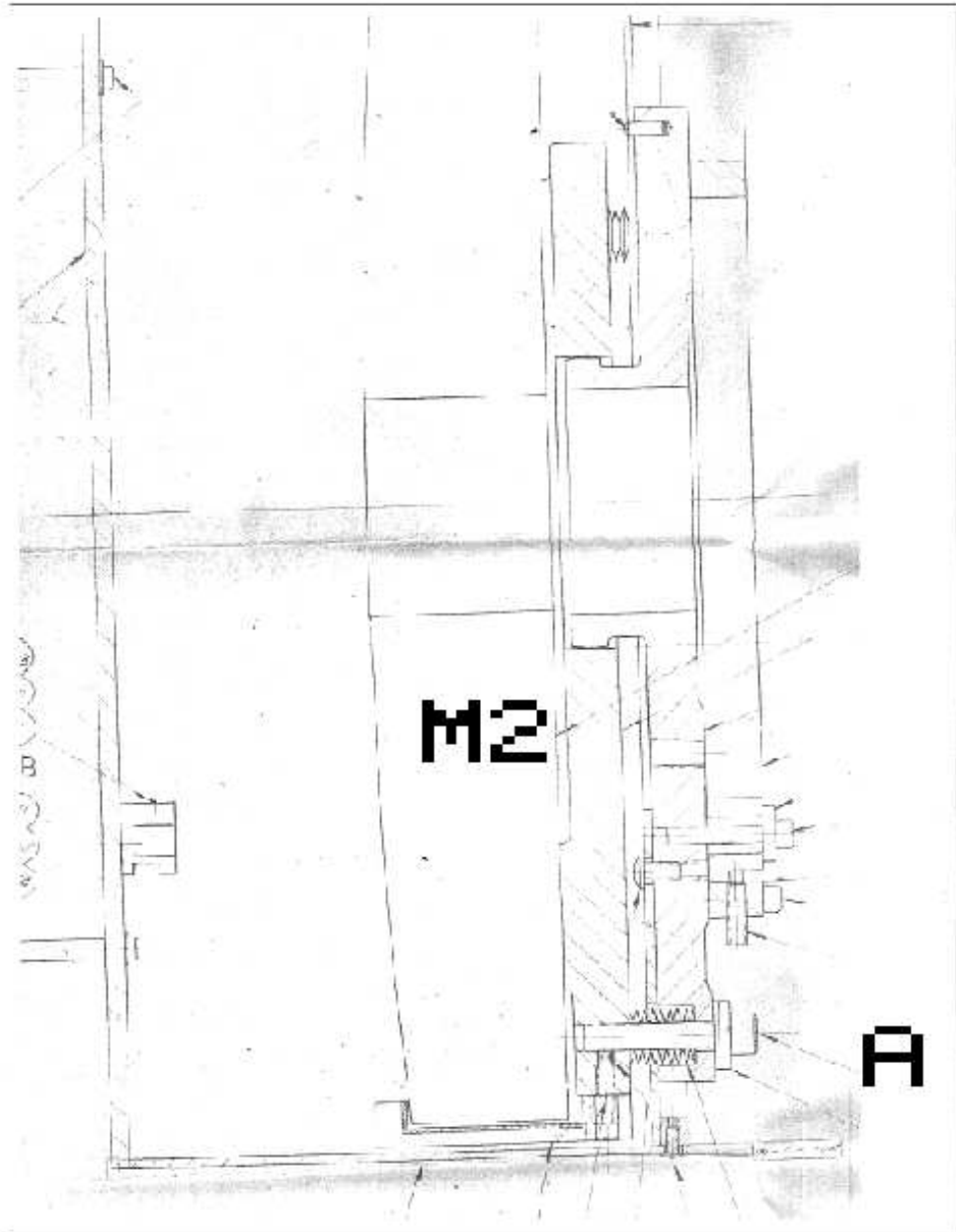


Fig. 2.—

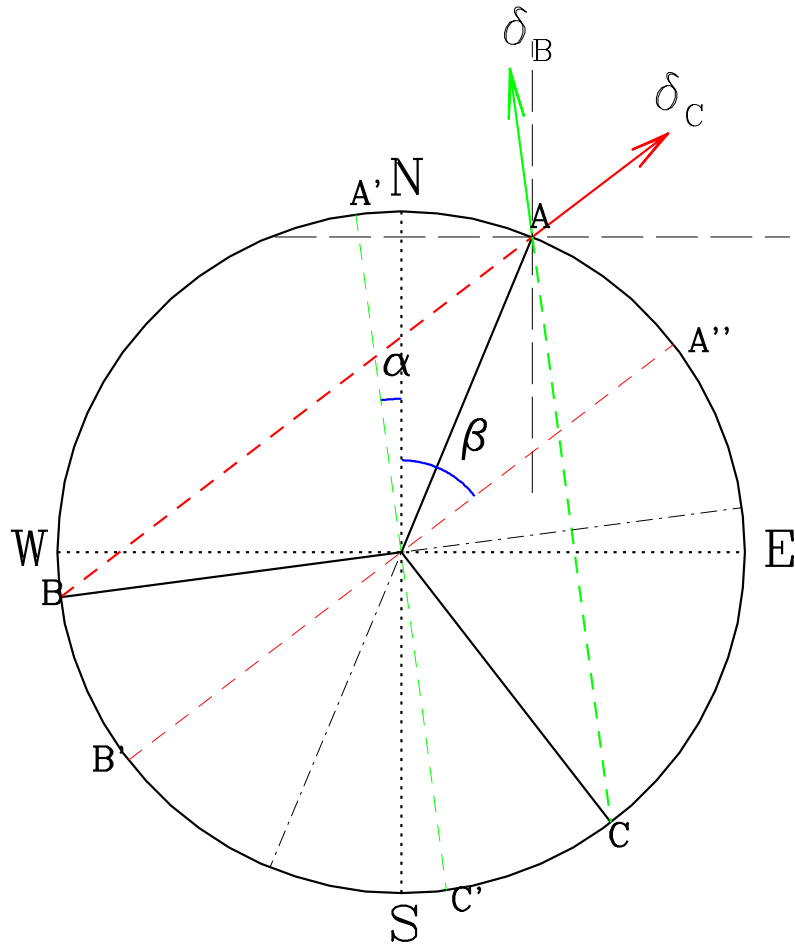


Fig. 3.—